

NEW GRADE OF SLEEVE MATERIAL WITH IMPROVED WEAR RESISTANCE FOR FINISHING STANDS



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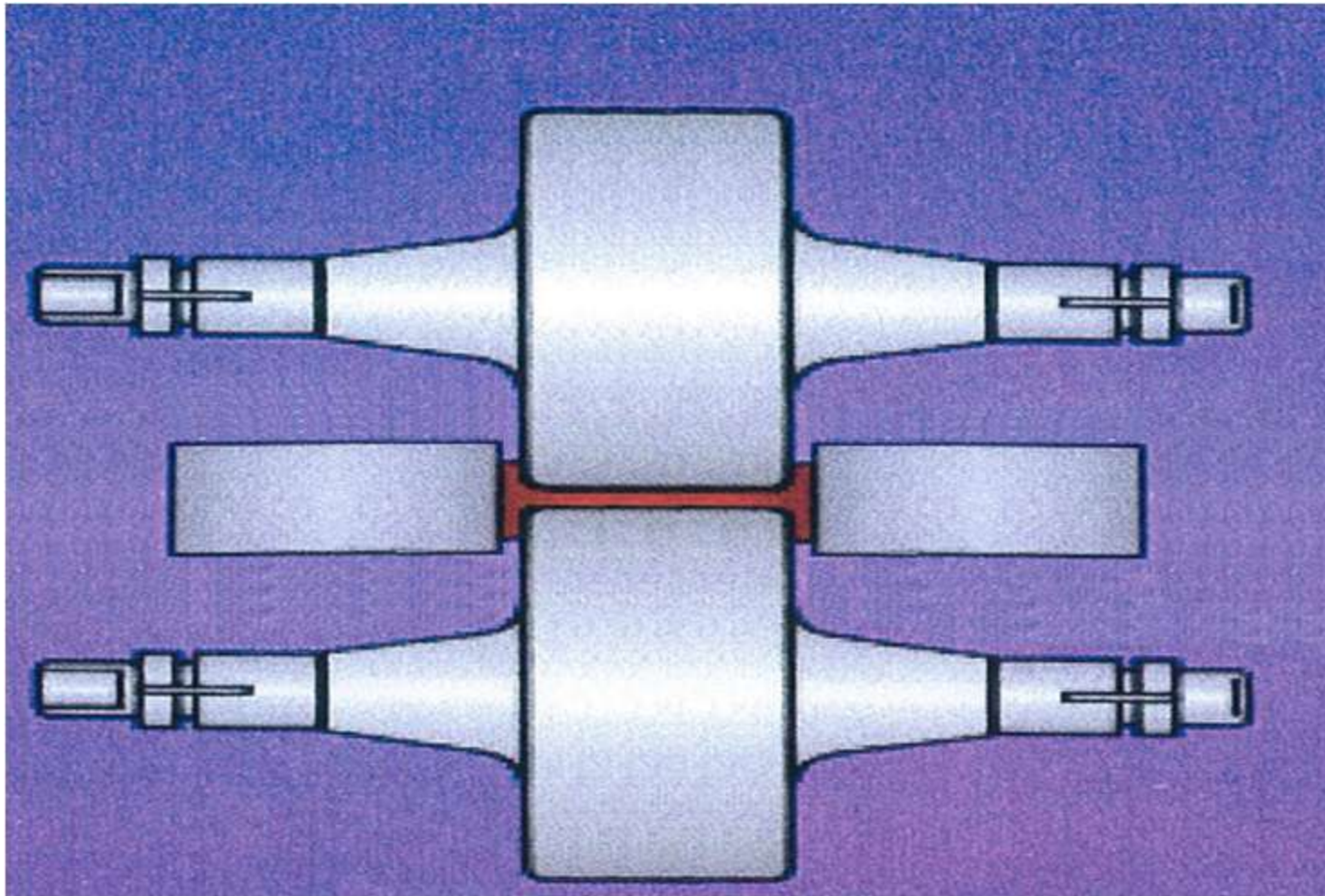
MCC International Inc.

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TOPICS COVERED

- **Principle Understanding of types of rolls**
- **Process of manufacture of sleeves**
- **Methodology of developing the new grade**
- **Differences between new grade and conventional sleeve material**
- **Field test results**

PRINCIPLE UNDERSTANDING BEAM MILL-UNIVERSAL STAND

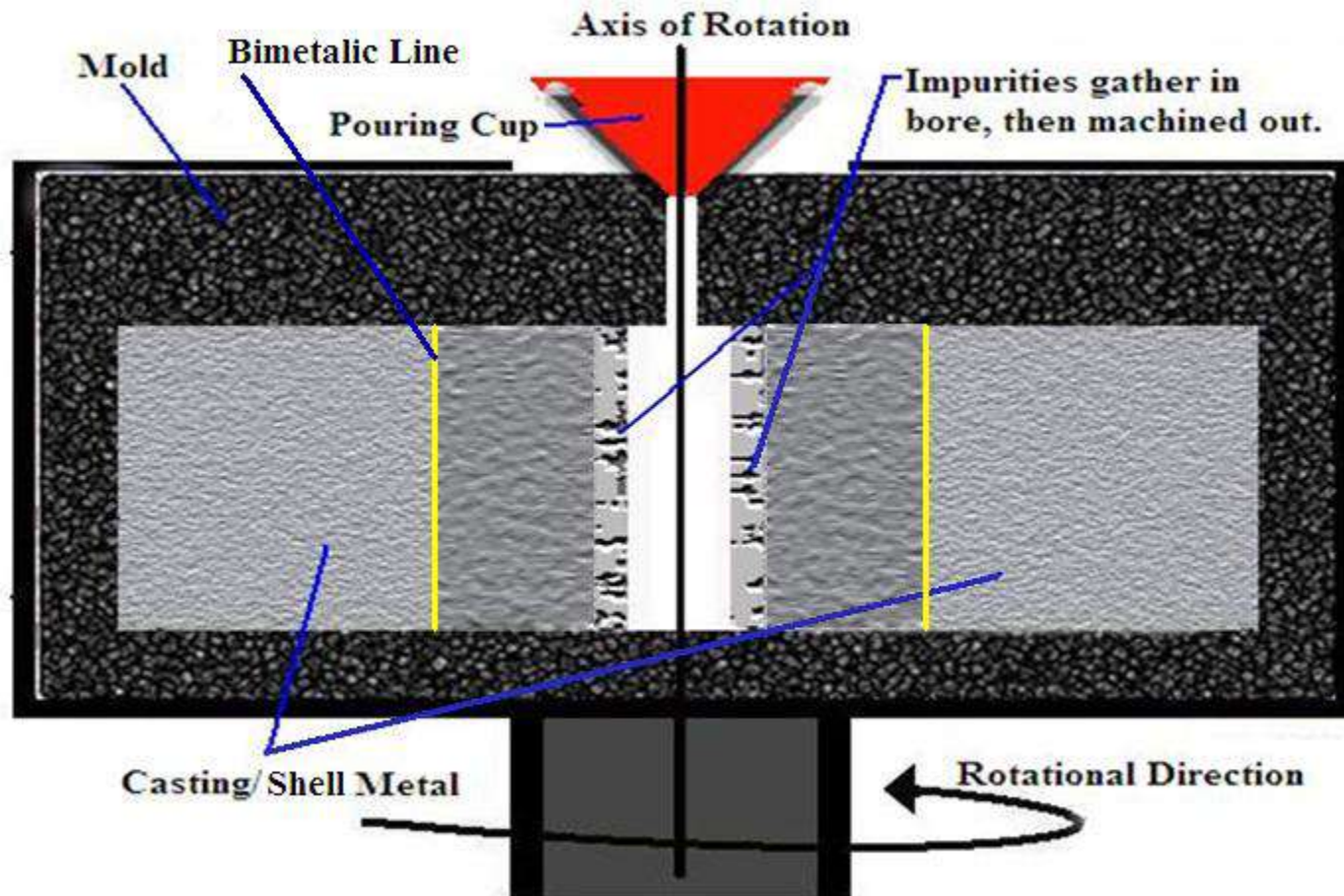


PRINCIPLE UNDERSTANDING DIFFERENT ROLL DESIGNS FOR BEAM MILLS

- **Single Poured solid (Monobloc) rolls
(Traditionally used)**
- **Two Piece Construction consisting of Forged steel arbor with a shrink fitted sleeve**
- **Sleeves double Poured with Harder outer shell and Softer inner core**



PRINCIPLE OF UNDERSTANDING SCHEMATIC OF VERTICAL CENTRIFUGAL CASTING PROCESS

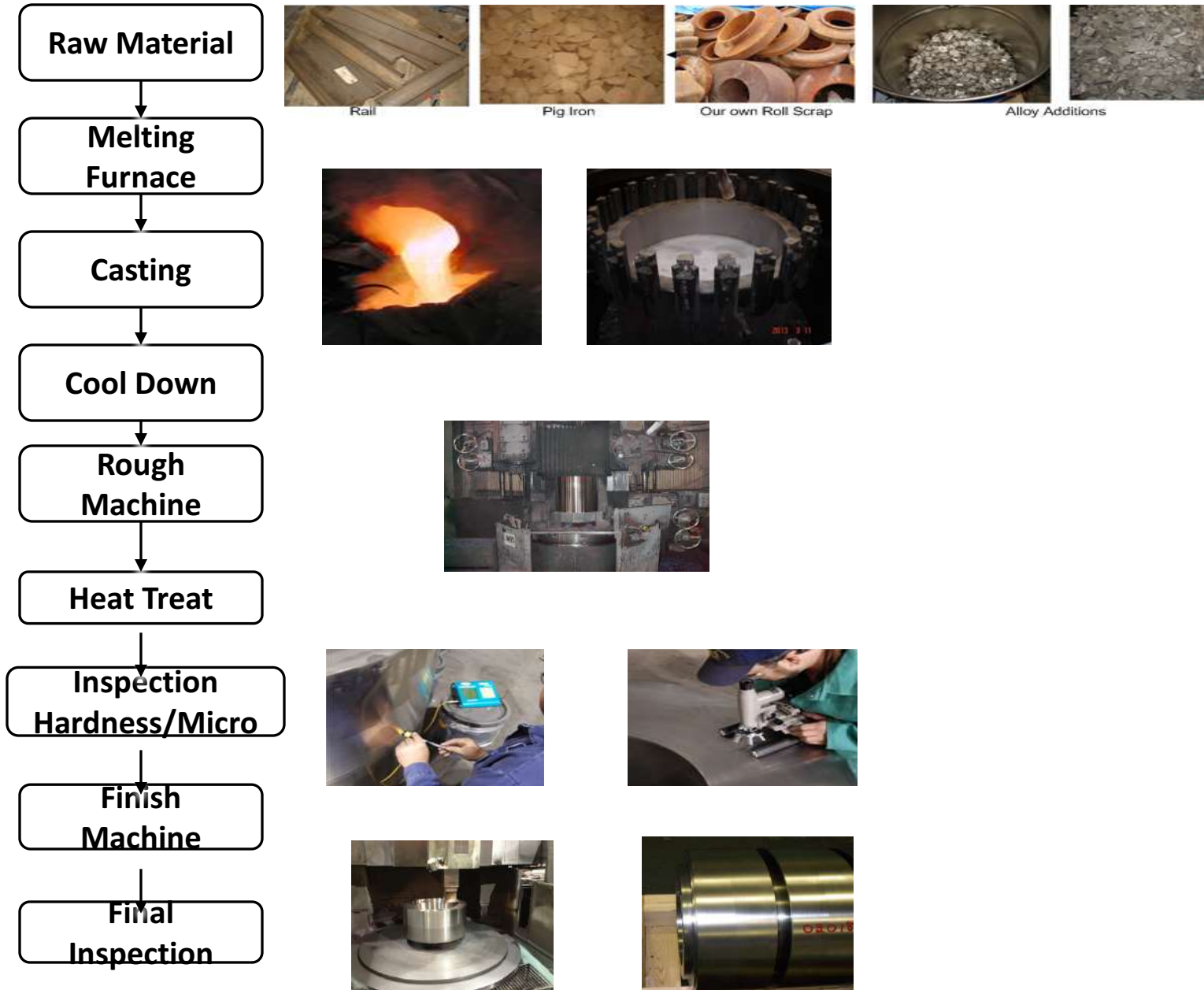


PRINCIPLE UNDERSTANDING ADVANTAGES OF CENTRIFUGAL CASTING

- **Directional solidification (OD to ID)**
- **Impurities are forced out inside bore & machined out**
- **Finer Grain Structure**
- **Casting Bimetal rolls with softer core**

PRINCIPLE UNDERSTANDING

MANUFACTURING PROCESS FLOW DIAGRAM



PRINCIPLE UNDERSTANDING THAT SUPPORT NEW MATERIAL

CONVENTIONAL HORIZONTAL ROLL MATERIALS

Grade	Typical Hardness Range, Shore C scale
Adamite	55-63
Nodular Iron	55-78
High Chrome Steel	66-73
HSS	75-85

METHODOLOGY: RECOGNIZING SHORT COMINGS

- **Customer experienced high wear rate at the later finishing stands using Adamite or Nodular Iron sleeve**
- **Traditional Adamite grade hardness (abrasive wear resistance) limited to 65-67 shore max.**
- **Traditional Nodular Iron grade hardness is limited to 70-72 shore max.**
- **Adamite & NI perform well during initial campaign but tend wear faster during later part of campaign.**

METHODOLOGY: MICRO CONSTITUENTS THAT AFFECT THE SLEEVE PERFORMANCE

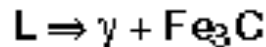
- **PERCENTAGE CARBIDES**
(Eutectic Carbides & Secondary Carbides)
- **TYPE OF CARBIDES**
(Iron Carbides, Chrome Carbides, Moly Carbides)
- **TYPE OF MATRIX**
(Pearlite, Bainite/Acicular)
- **GRAPHITE**
(Morphology of Graphite)

IRON- CARBON PHASE DIAGRAM

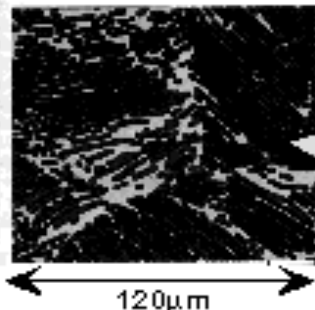
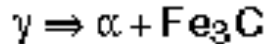
Iron-Carbon (Fe-C) Phase Diagram

- 2 important points

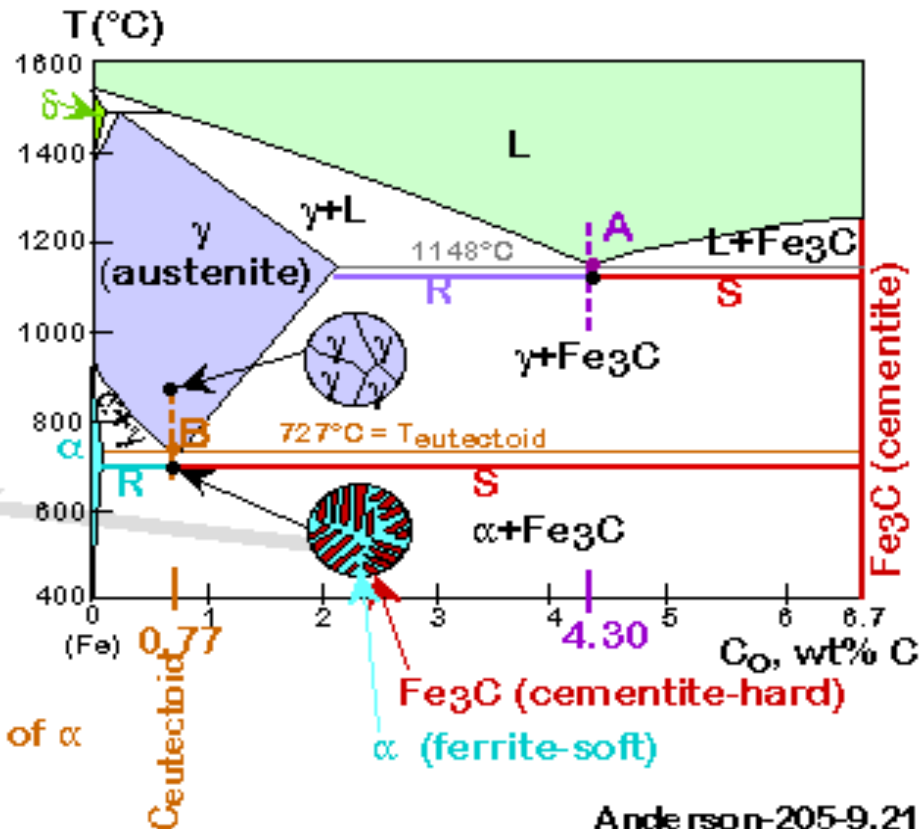
-Eutectic (A):



-Eutectoid (B):



Result: Pearlite = alternating layers of α and Fe_3C phases.



Anderson-205-9.21

$$w_{\text{pearlite}} = 1$$

METHODOLOGY: UNDERSTANDING THE CAUSES OF SHORTCOMINGS

Adamite Grade:

Carbon Content: 1.5 to 2.2 %

Amount of Primary/Eutectic Carbides form during solidification is Restricted to about 20 %

Nodular Iron Grade:

Carbon Content: 3.0 to 4.0 %

Nodular Irons have higher percentage of Eutectic carbides (25 to 33 %). They have softer matrix (Pearlite or upper Bainite)

METHODOLOGY: ESTABLISHING THE OBJECTIVES FOR THE NEW GRADE

The Composition and Processing are Selected to provide:

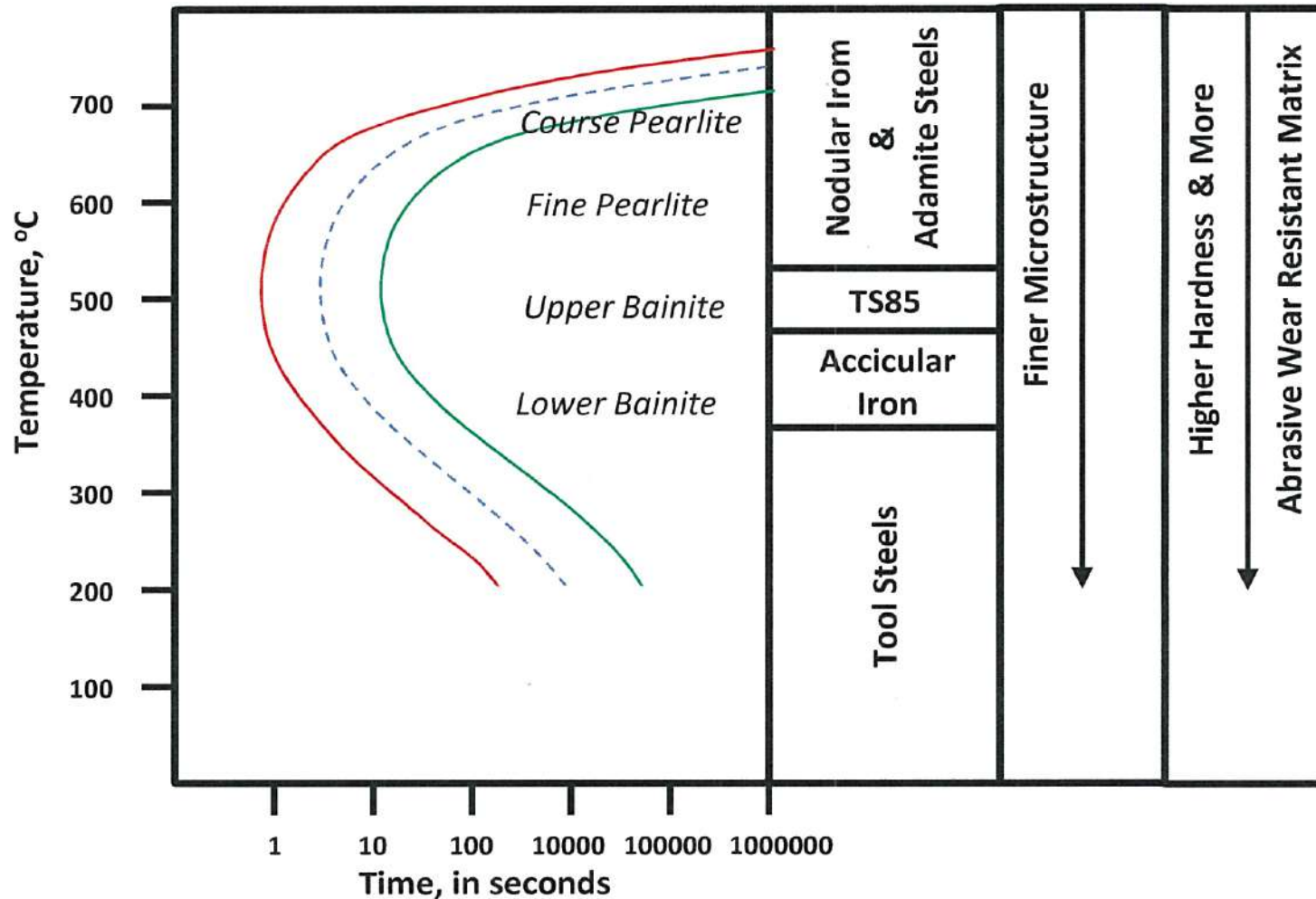
- **Optimum Amount of Eutectic Carbides**
 - **Special Secondary Carbides**
 - **Harder and Tougher Matrix**

DIFFERENCES IN CHEMICAL COMPOSITION ADAMITE, NODULAR IRON & NEW GRADE

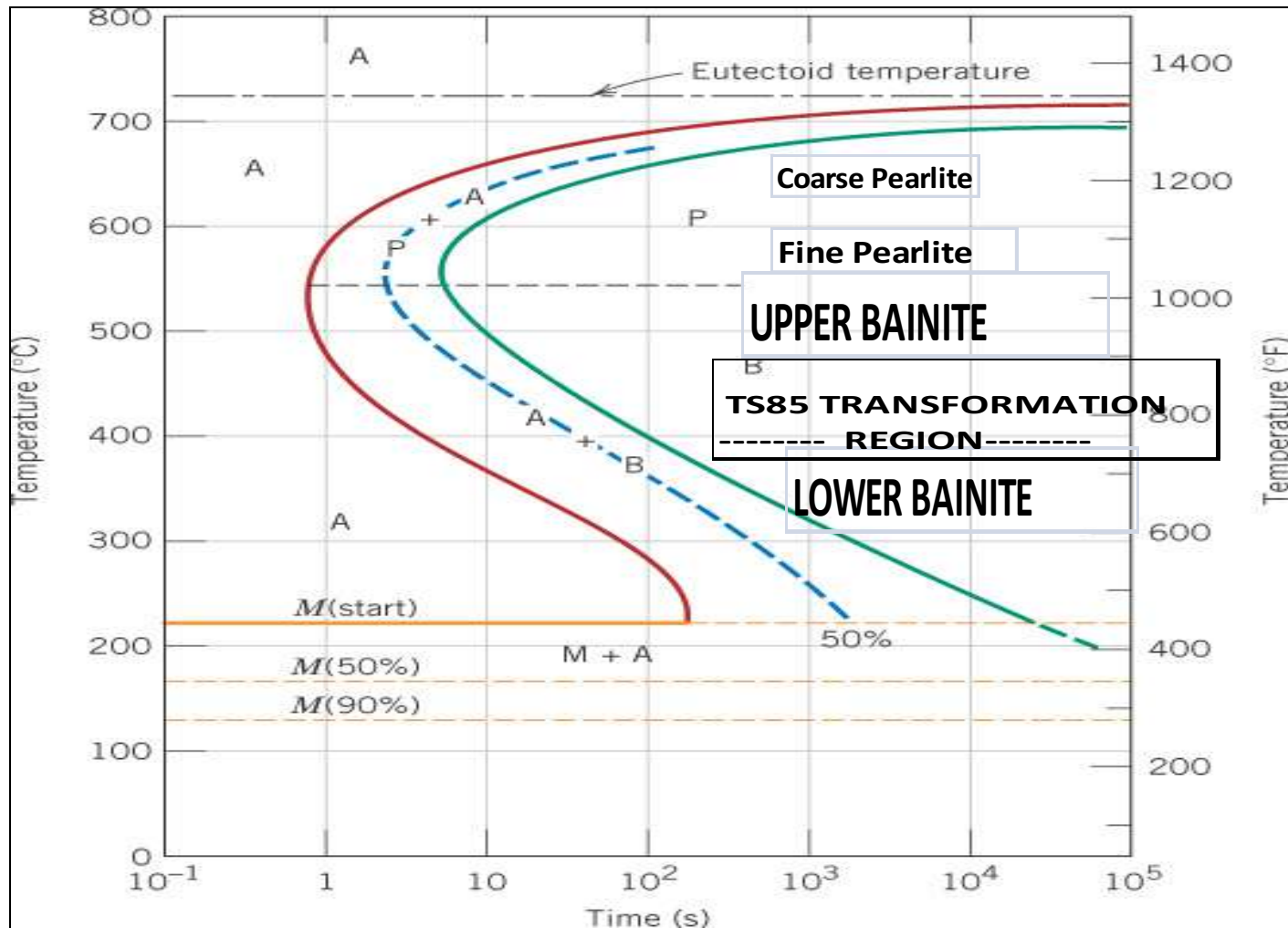
Grade	C	Si	Mn	Cr	Ni	Mo	Others
Adamite	1.50-2.30	0.50- 0.90	0.5-1.00	1.00 -4.30	1.00- 1.50	0.15- 0.50	---
Nodular Iron	3.00- 3.40	1.30-2.10	0.30-0.70	0.15-0.90	1.90-2.50	0.15-0.50	---
New Grade TS85	1.90- 3.30	0.50-1.50	0.30-1.00	0.50-2.00	2.00-5.00	0.15- 1.00	Nb, V,W upto 2.00

DIFFERENCES: MATRIX TRANSFORMATION

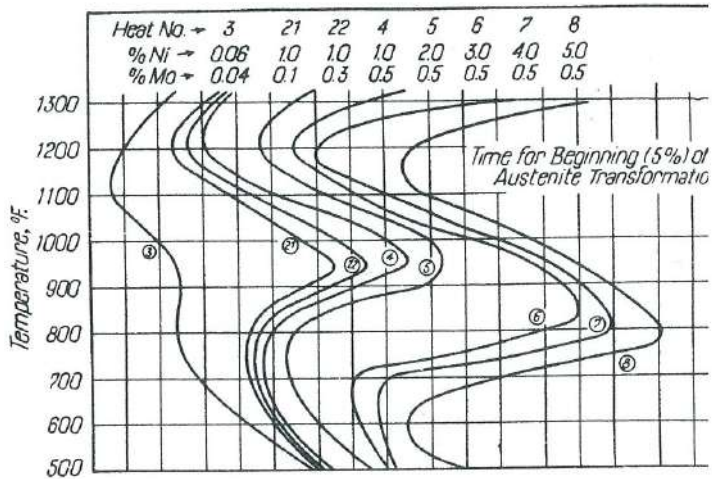
SCHEMATIC TTT DIAGRAM



DIFFERENCES: TS85 MATRIX TRANSFORMATION REGION



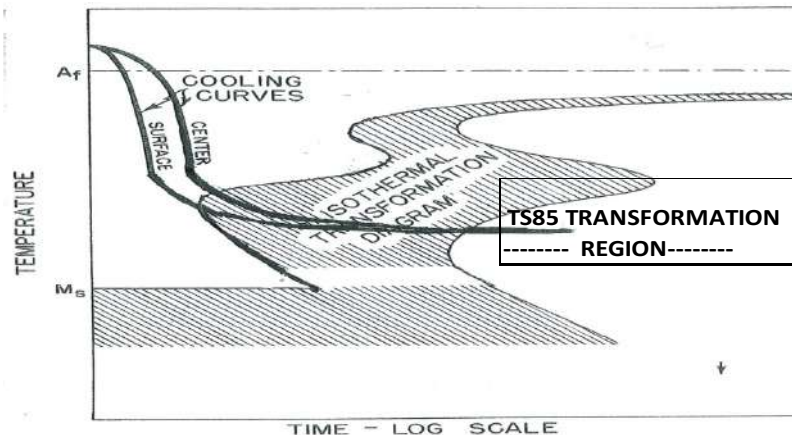
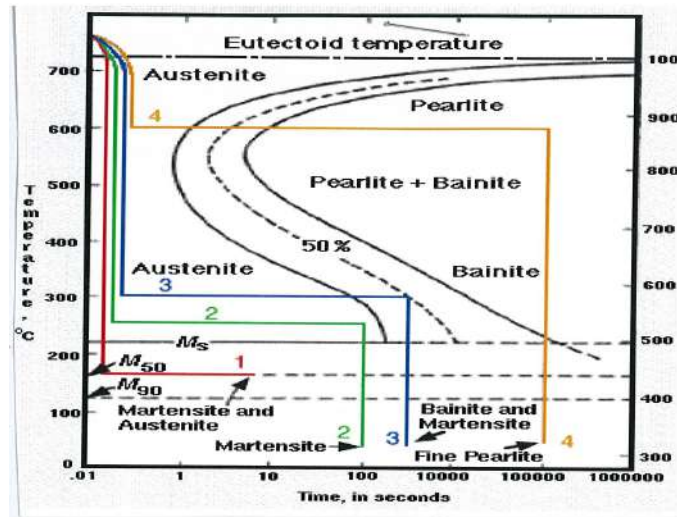
CONTROL OF COMPOSITION AND COOLING TO ACHIEVE THE DESIRED TRANSFORMATION



2nd curve left (#21) 1% Ni, 0.1 Mo

Right extreme curve (#8) 5% Ni, 0.5 Mo

TTT diagram with 2.5 C,
2% Si

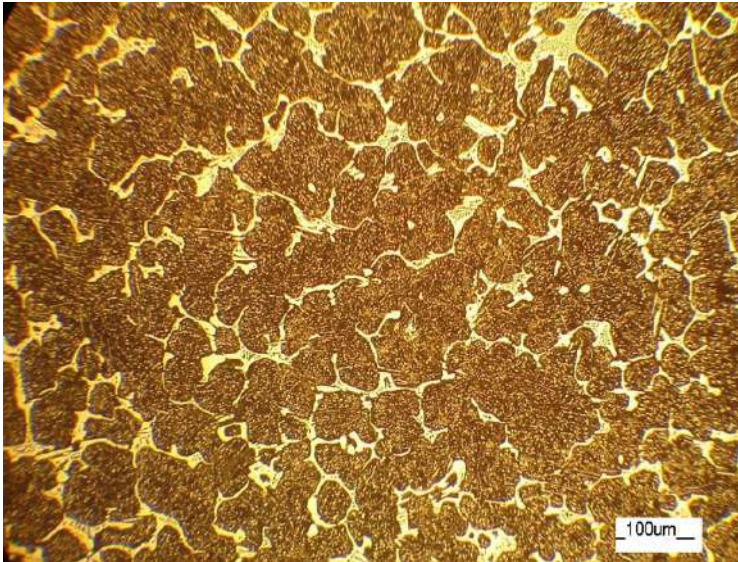


DIFFERENCES: SPECIAL CARBIDES

MICRO HARDNESS & CRYSTAL STRUCTURE OF VARIOUS CARBIDES

Carbide	Micro Hardness (Vickers Scale)	Crystal structure
Fe(3)C	800- 1090	Orthorhombic
(Fe Cr) ₃ C	850- 1370	Orthorhombic
Mo(2)C	1500-1650	Hexagonal
NbC	2400	Cubic
Cr(3) C(2)	1300	Orthorhombic
VC	2400- 2600	Hexagonal

DIFFERENCES: CARBIDE CONTENT MICROSTRUCTURE OF ADAMITE & NEW GRADE



Microstructure of Adamite
100 X 2% Nital AS100*

Est. % of Primary/Eutectic carbides = 18 %



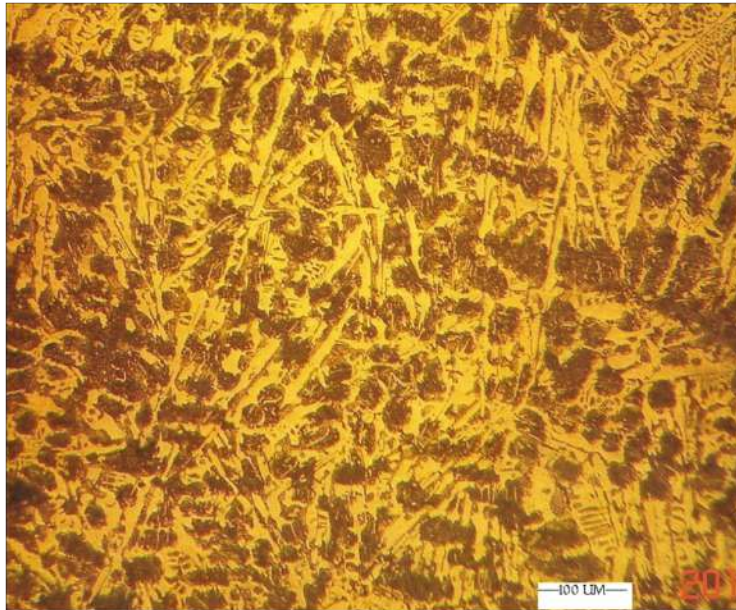
Microstructure of TS85*
100 X 2% Nital

Est. % of Primary/Eutectic carbides = 33 %

*AS100 is MCC International trade name for Adamite

TS85 is MCC International trade name for new grade

DIFFERENCES: CARBIDE CONTENT MICROSTRUCTURE OF NODULAR IRON & TS85



**Microstructure of Nodular
Iron Roll**

NI70*

% of Primary/Eutectic carbide= 24 %
(100 x 2% nital etch)

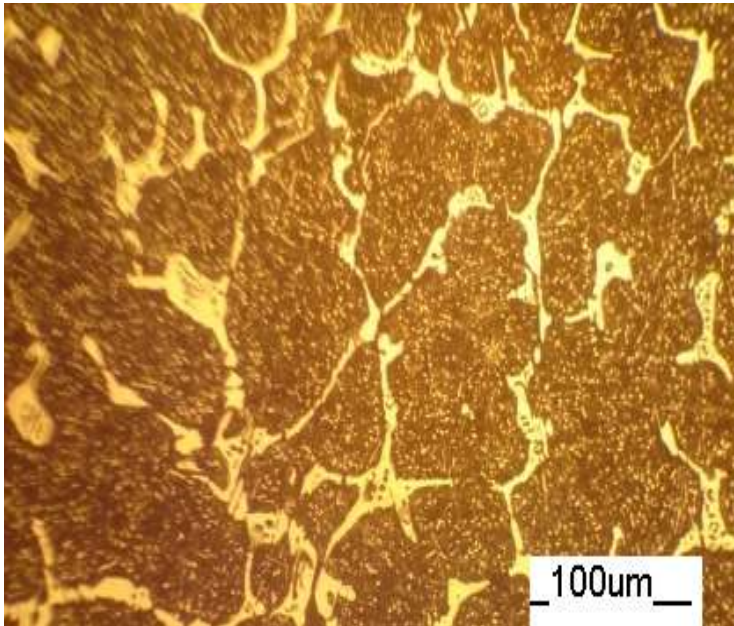


**Microstructure of TS85
Roll**

% of Primary/Eutectic carbide= 33 %
(100 x 2% nital etch)

*NI70 is MCC International trade name for Nodular Iron (70 Sh.)

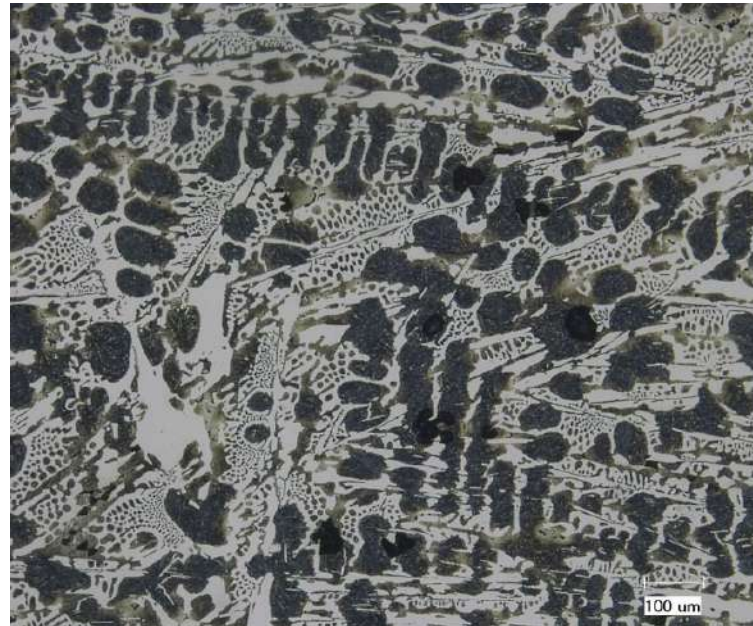
DIFFERENCES: MICROSTRUCTURAL DIFFERENCES OF ADAMITE & TS85*



Microstructure of Adamite

200 x

2 % Nital etch



Microstructure of TS85

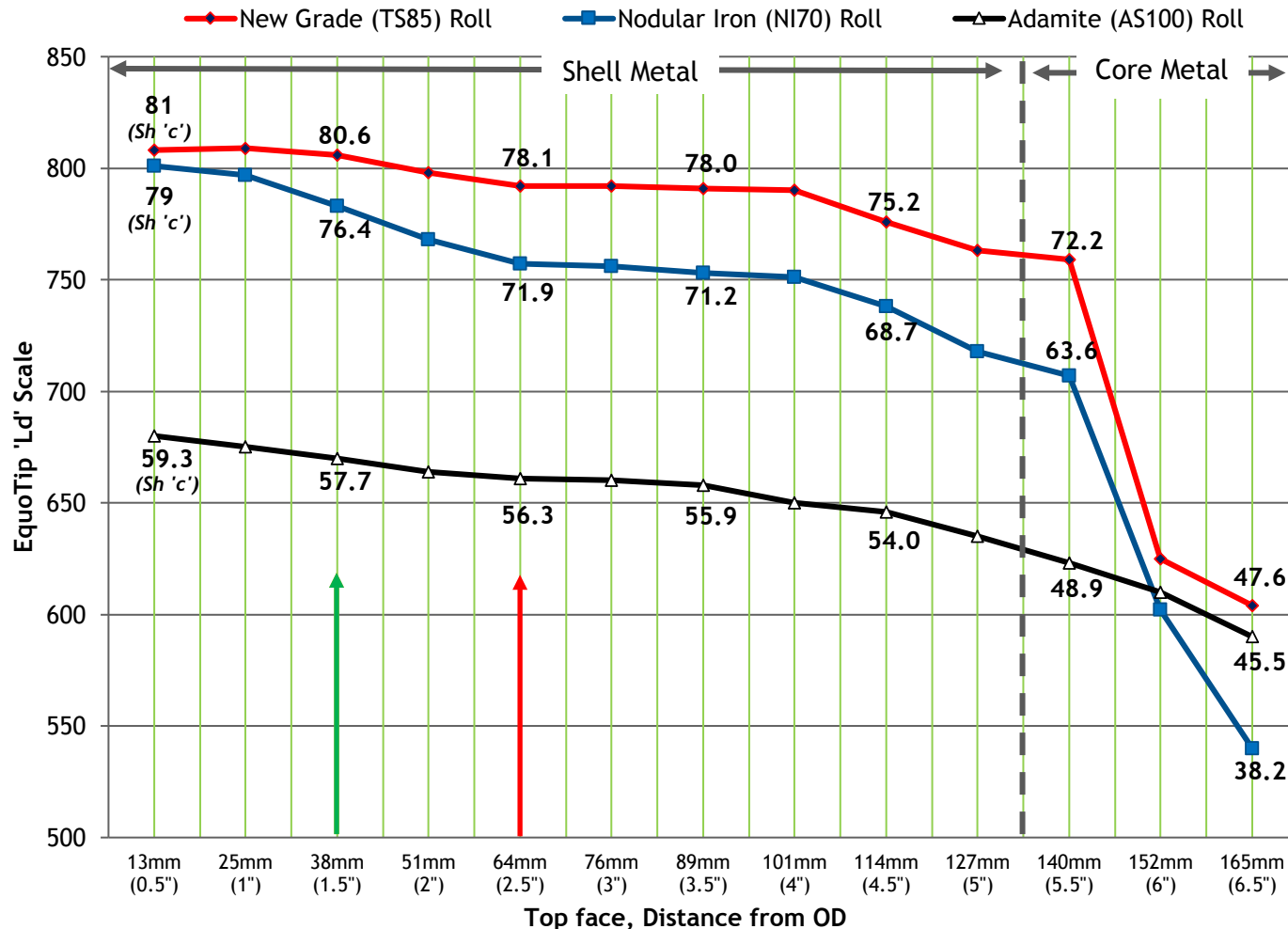
200 x

2 % Nital etch

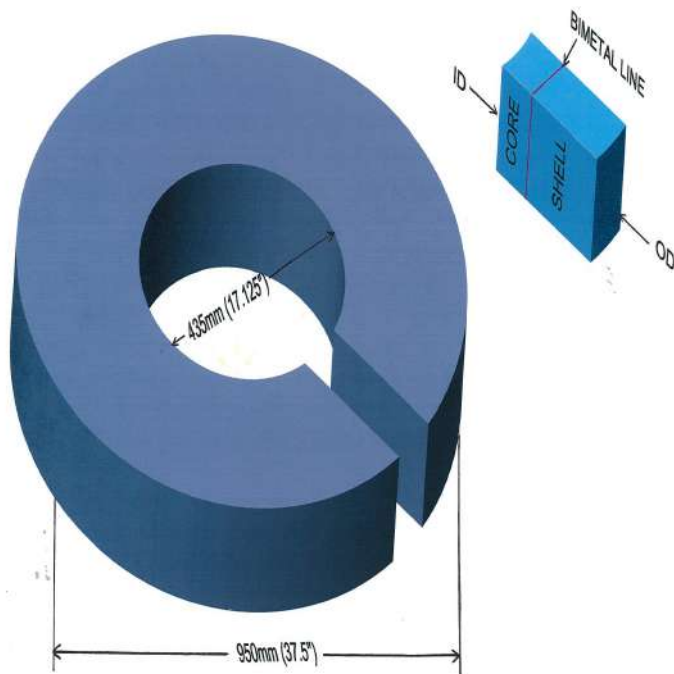
TS85 is MCC International trade name for new grade

DIFFERENCES: HARDNESS DATA ADAMITE, NI & TS

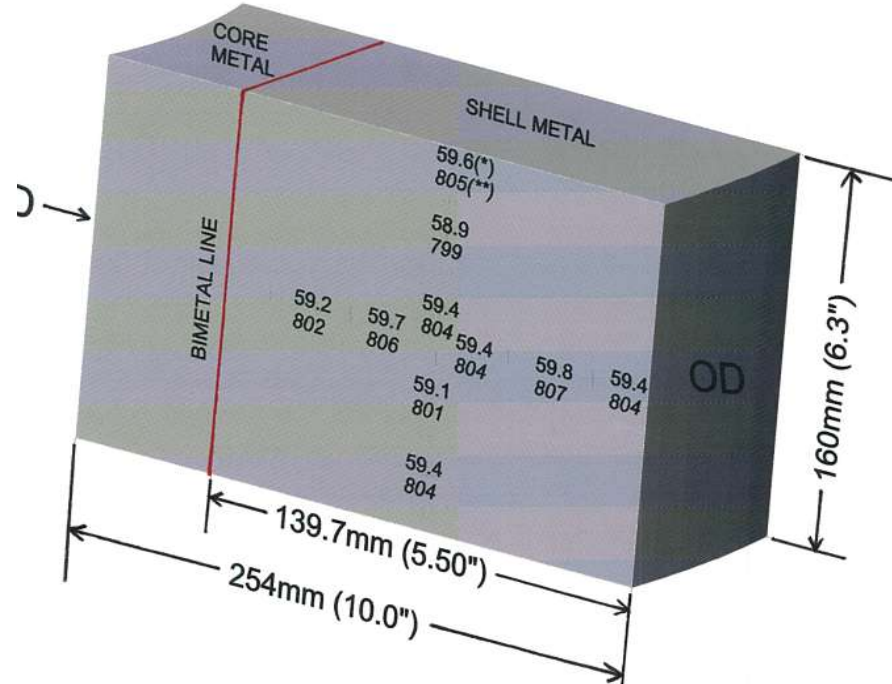
COMPARISON OF HARDNESS PROFILE ON THE FACE



SCHEMATIC OF SAMPLE FOR MICRO AND HARDNESS

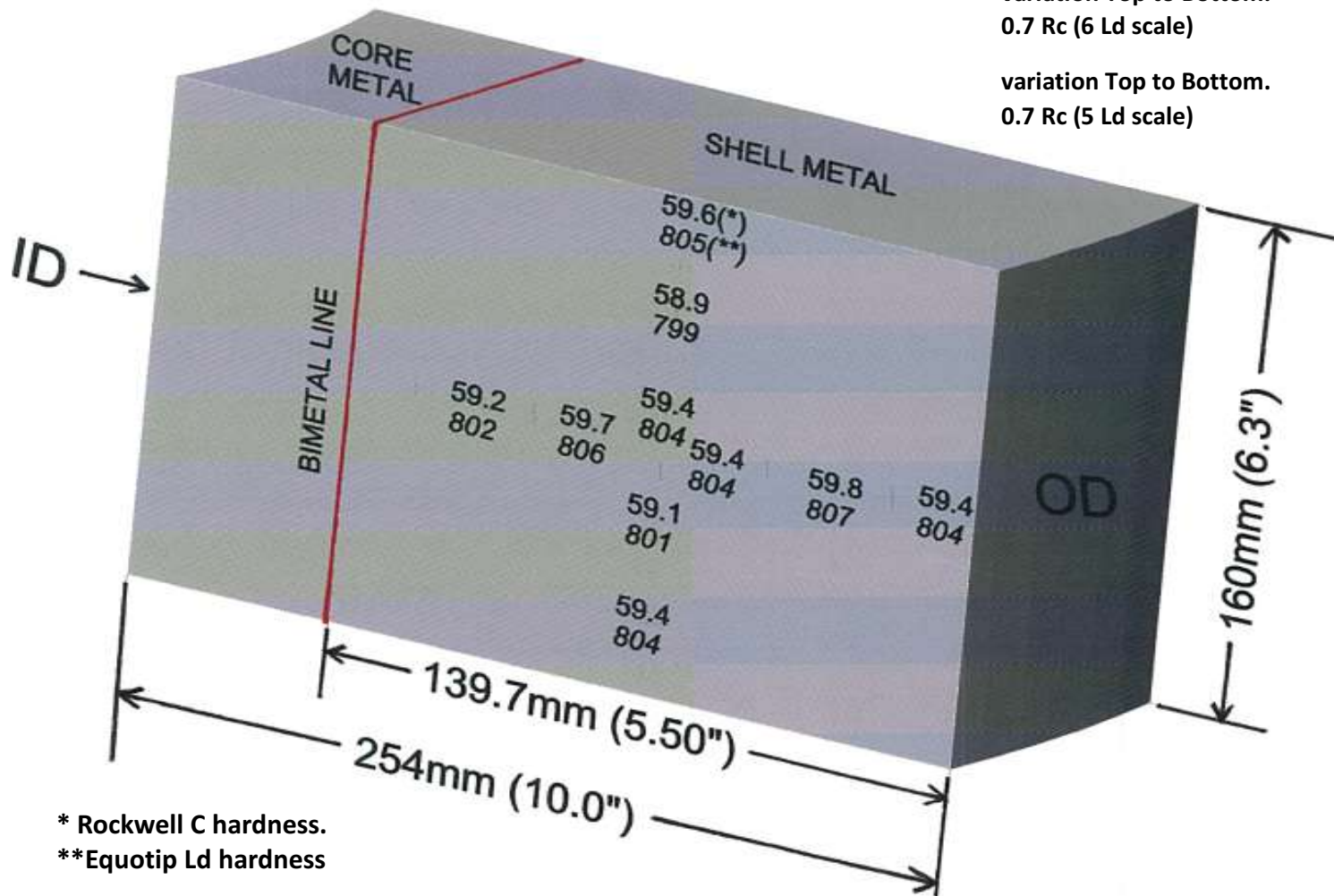


Schematic of sample cut from the roll for hardness & micro.



Hardness reading from Top face to bottom face & thru' the wall thickness.

DIFFERENCES: HARDNESS DATA THRU' THE SECTION THICKNESS



* Rockwell C hardness.

** Equotip Ld hardness

RESULT: SUCCESSFUL APPLICATION FILED TESTING _PROCESSING W6X6 BEAM



Stands 7-12 with a W6x6 in them

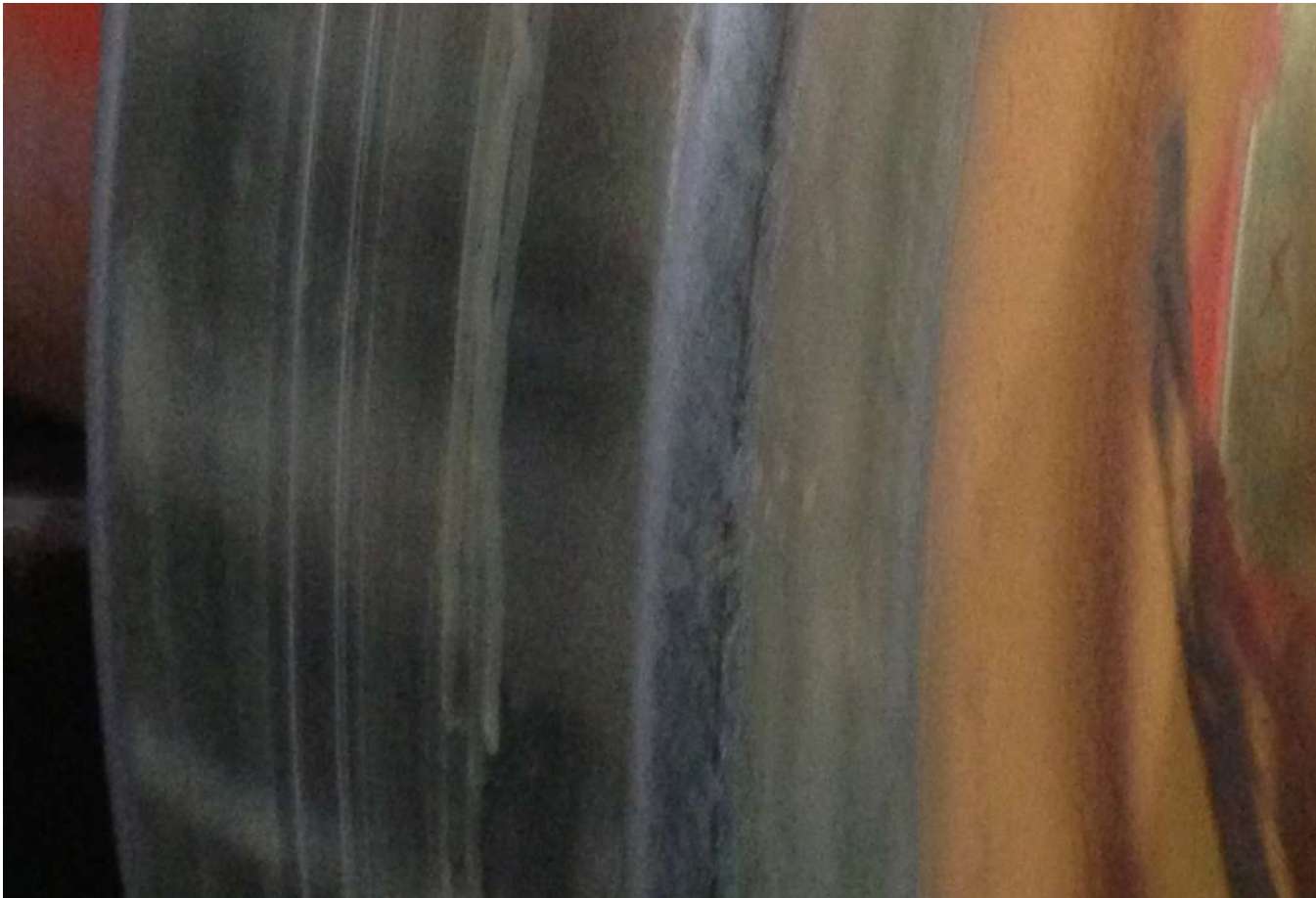
**RESULT: MINIMUM WEAR ON SLEEVE SURFACE.
TS85 ROLL WEB AT 500 TONS, JUST STARTING TO
WEAR, BUT STILL HAS LATHE MACHINING MARKS.**



**RESULTS: MINIMUM DEGRADATION AFTER 1000 TONS.
TS85 SLEEVE WEB STILL LOOKS GOOD. THE SCALE
WILL BREAK AFTER THE STRAIGHTENER**



**RESULTS: FINISHER ROLL AFTER 1123 TONS.
TS85 SLEEVE CHANGED ONLY BECAUSE IT HAD
A GUIDE MARK IN THE CENTER OF THE PASS.**



**RESULTS: NO MARKINGS ON THE FLANGE SURFACE.
W6 X6 FLANGE SURFACE AFTER PROCESSING 1000 TONS**



Surface looks very good except for light scale & water marks

RESULTS: COMPARISON OF DRESSING REQUIRED. AVERAGE ROLLING CAMPAIGN & AMOUNT OF DRESSING FOR ADAMITE, NODULAR IRON & TS85

Sleeve material	Average tons/ rolling	Amount of dressing for clean up
Adamite*	425	15-20mm
Nodular Iron **	1000	8 mm
New grade (TS85)	1150	4-5 mm

* MCC AS100 Grade.

**MCC NI70 Grade.

RESULTS: FLANGE DIMENSIONAL CONSISTANCY. LASER BAR GAGE SHOWS HOW CONSISTENT ARE THE FLANGE WIDTH



RESULTS: SUCCESSFUL APPLICATION BEAM COMING OUT FINISHING STAND



SUMMARY

- ❖ An overview of Vertical Centrifugal Casting is provided.
- ❖ Limitation of Conventional Sleeve (roll) material is explained (Carbide content, matrix)
- ❖ The chemistry range and the final microstructure of the new Grade (TS85) is provided
- ❖ The hardness profile for the new Grade is compared with Traditional Adamite and Nodular Iron grades
- ❖ The field test results of the sleeve performance is provided.

CONCLUSIONS

- ❖ The test results show when rolling w6 x6 beam using the new material grade (TS85*), required 70% less dressing compared to conventional Adamite Sleeve and 50% less compared to Nodular Iron grade.
- ❖ By replacing conventional sleeves (Adamite/ Nodular iron) with TS85 customer achieved the following:
 1. LESS ROLL DRESSING BETWEEN CAMPAIGN
 2. REDUCED THE NUMBER OF ROLL CHANGES
 3. MINIMIZED ROLL ADJUSTMENTS DUE TO MORE CONSISTANT BAR
 4. IMPROVED PRODUCTIVITY

* TS85 is MCC International trade name for the new grade.

FINAL REMARK

- ❖ Hardness is only one part of equation for improved performance(optimum micro-structure provides significant improvement in fire cracking and fatigue resistance)
- ❖ Changing the sleeve at the same interval or taking same amount of dressing defeats the purpose of new and improved roll materials
- ❖ Keeping good data on rolling campaign (tonnage, dressing) is the key for increased Mill Productivity.

© **THANK YOU ALL**

SEM PICTURE SHOWING THE SPECIAL SECONDARY CARBIDES IN THE MICRO

